Coating	Source	Description	Billet Material Treated
C1	Commercial	Zinc phosphate coating	AISI 4340
C2	Battelle	Fluoride-phosphate coating	Ti-6Al-4V
C3	Battelle	Metal-free phthalocyanine	AISI 4340
C4	Battelle	Lead coating	AISI 4340
C5(a)	Watervliet Arsenal	Anodized coating	Ti-6Al-4V
C6(a)	Battelle	Diffused nickel-plating	Ti-6Al-4V

TABLE IV.BILLET CONVERSION COATINGS EVALUATED IN THEHYDROSTATIC-EXTRUSION PROGRAM

(a) C5 and C6 were numbered in the Interim Reports as C3 and C4, respectively, in error. However, duplication of coating numbers did not occur in the individual reports.

As a contrast, however, Coating C5 was always necessary in the cold hydrostatic extrusion of Ti-6Al-4V alloy at room temperature. Without C5, severe lubrication breakdown occurred often and resulted in a poor quality product. However, at 500 F, it was not necessary to use coatings with this alloy; excellent lubrication was obtained with billet lubricant (L33) alone.

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CHARACTERISTICS OF PRESSURE-DISPLACEMENT CURVES

The effectiveness of lubrication systems in hydrostatic extrusion is evaluated by comparing extrusion pressures, extruded surface finishes, and the general characteristics of the pressure-ram displacement curves produced during extrusion. The pressurecurve characteristics were found to differ considerably for different lubricant systems and billet materials.

It has been found that the extrusion pressure-displacement curves can be classified into families as shown in Figure 26. That figure is placed at the end of the text in Section 1 on a foldout page for ready reference when the extrusion data are being examined. Each family of curves is designated by a letter, and the number following it classifies the typical runout characteristics within each family.

Curves Types A, B, C, and D represent quality of lubrication in decreasing order of effectiveness. These curve types have been numerically classified further according to the following characteristics during runout:

Number	General Runout Characteristics	
1	Constant	
2	Decreasing	
3	Increasing	
4	Special	

<u>Type A Curves</u>. One of the aims of the experiments on lubrication systems in the program was to obtain conditions giving a curve of Type A 1 which represents completely effective lubrication throughout the extrusion stroke. Experience has shown that once this type of curve is achieved, for a given material and extrusion ratio, other lubrication systems may not lower the value of P_r (runout pressure) markedly and therefore the curve very likely represents near-optimum lubrication conditions. There is no break-through pressure (P_b) peak above the runout pressure which suggests that the static friction, μ_s , is about the same as the kinetic friction coefficient, μ_k , developed once the billet starts to move.

The runout characteristics in the other Type A curves may represent partial lubrication breakdown due to pressure-temperature effects at the billet-die interface or changes in flow strength due to adiabatic heating of the billet.

<u>Type B Curves</u>. All the curves in this category are generally characterized by a rounded breakthrough pressure peak (P_b) followed by a smooth runout curve at a lower pressure (P_r). The occurrence of a rounded pressure peak has been attributed to the fact that μ_s is somewhat higher than $\mu_k^{(1)}$, but not sufficiently to cause a sharp stickslip peak. In some cases, the breakthrough pressure peak is sharp, indicating a stickslip situation at breakthrough only.

<u>Type C Curves</u>. These curves are similar to Type B curves except that one or a few cycles of stick-slip follow the breakthrough pressure peak. Here stick-slip is generally not severe, its amplitude decreasing to give a smooth runout curve.